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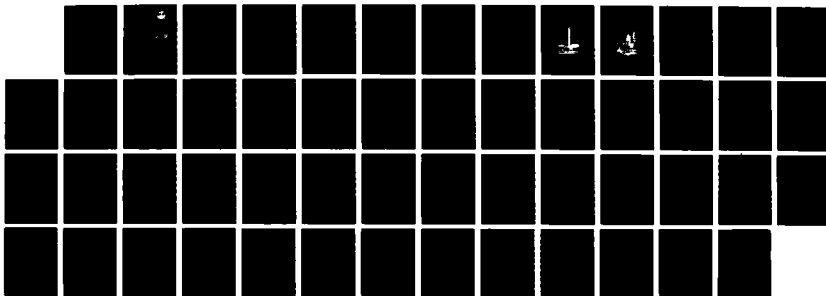
STACK EMISSION TESTING FOR BERYLLIUM HILL AFB UTAH(U)
AIR FORCE OCCUPATIONAL AND ENVIRONMENTAL HEALTH LAB
BROOKS AFB TX N DALY NOV 87 USAFOEHL-87-144EQ0086LEF

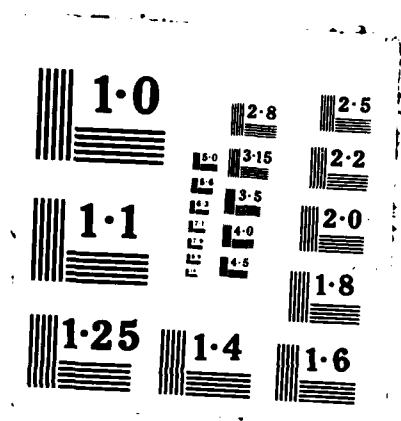
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USAFOEHL REPORT
87-144EQ0086LEF



STACK EMISSION TESTING FOR BERYLLIUM,
HILL AFB UT

MARY M. DALY, Capt, USAF, BSC

November 1987

Final Report

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USAF Occupational and Environmental Health Laboratory
Human Systems Division (AFSC)
Brooks Air Force Base, Texas 78235-5501

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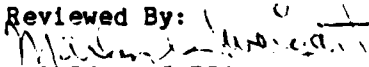

JOHN J. COUGHLIN, Colonel, USAF, BSC
Commander

Prepared By:


MARY M. DALY, Capt, USAF, BSC
Consultant, Air Quality Engineer

Reviewed By:


JAMES A. GARRISON, Major, USAF, BSC
Chief, Air Quality Function

Reviewed By: 
MARTIN L. SWEIGART, Lt Col, USAF, BSC
Chief, Environmental Quality Branch


SHELTON R. BIRCH, Colonel, USAF, BSC
Chief, Consultant Services Division

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		Stack sampling Hill C-5	
		Stack emission(s) Beryllium brake shop	
19. ABSTRACT (Continue on reverse if necessary and identify by block number) At the request of HQ AFLC/SGB, personnel from the USAFOEHL conducted an air emission survey of the exhaust from a C-5 brake reconditioning operation at Hill AFB UT from 13 July to 17 July 1987. These brakes contain beryllium disks and during the reconditioning process, beryllium particles are generated. The reconditioning operation consists of two processes which vent to individual stacks. The emissions for both stacks were well below the EPA standard for this kind-of operation.			
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22a. NAME OF RESPONSIBLE INDIVIDUAL Capt Mary Daly		22b. TELEPHONE (Include Area Code) (512) 536-2891	22c. OFFICE SYMBOL ECQ

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I. INTRODUCTION

On 13-17 July 1987, stack emission sampling of the exhaust from the C-5 brake reconditioning operation in Bldg 507 was accomplished at Hill AFB UT. These brakes contain beryllium disks and, during the reconditioning process, beryllium particles are generated. The survey was requested by HQ AFLC/SGB to determine the amount of beryllium being exhausted from the facility. Testing was conducted by the Air Quality Function of the USAF Occupational and Environmental Health Laboratory (USAFOEHL). Sampling team members are listed in Appendix A.

II. DISCUSSION

A. Background

The brake shop conducts a two-part reconditioning operation on C-5 beryllium brake discs. This operation consists of an active wet grinding process and a wet dipping process. The reconditioning process is a cyclic operation for six hours per day and the shop operates only one shift per day. Each process is exhausted through its own stack and has no air pollution control equipment.

B. Applicable Standards

The national Environmental Protection Agency (EPA) emission standard for beryllium applicable to stationary sources is found in Chapter 40, Code of Federal Regulations, Part 61.30 (40 CFR 61.30). This standard limits beryllium emissions to not more than 10 grams over a 24-hour period. The State of Utah defers to the standard established by the EPA.

C. Site Description

The process for reconditioning the beryllium disks of the C-5 brake assembly is: (1) dipping in a sodium hydroxide solution, (2) glass bead blasting, and (3) re-dipping in the solution. Both the blasting and the dipping processes occur in closed rooms with restricted access. The dipping tanks are exhausted directly to the atmosphere through a stack on the roof (referred to in this report as the east stack). The blasting is done in a sealed cabinet with attached gloves (glove box or hood) to manipulate the brake disks. The exhaust is passed through a stainless steel filter with a water spray, primarily to recover the glass beads, and then exhausted through a second stack on the roof (referred to as the west stack). Both exhaust stacks on the roof were sampled. Both stacks are similar with a diameter of 15.75 inches and an example of one is shown in Figure 1.

D. Testing Methodology

All sampling and analysis for beryllium were done according to the procedures contained in 40 CFR 60-61, Methods 1-5, and 104. Sampling ports were located 2.5 feet downstream and 2 feet upstream from air flow disturbances in accordance with EPA Method 1. Figure 2 shows a photograph of the sampling equipment and personnel at the site with a detailed schematic of

the Method 5 sampling train shown in Figure 3. A performance test on each stack consisted of the average of three two-hour sample runs with the sampling probe positioned at 25, 50 and 75 percent of the duct diameter.

Prior to sampling, preliminary velocity, stack temperature, and cyclonic flow checks of the flue gas were determined according to EPA Methods 1 and 2. These data are included in Appendixes B and C. The data from the preliminary evaluations were used to determine the sampling nozzle size necessary to satisfy isokinetic conditions.

Quality assurance testing was accomplished by calibration of: (1) nozzle diameter; (2) triple beam balance (to measure within 0.5 g); (3) meter box; (4) post test meter box; and (5) pitot tube (coefficient assigned, C_p 0.84). These data are included in Appendix D.

E. Results

Table 1 presents the results obtained during stack testing of the brake reconditioning operation. Results indicate that the beryllium emission rate from the east stack (exhausts dipping operation) was less than 0.028 grams per day (g/d) based on a detection limit of 1.25 micrograms. The emission rate from the west stack (exhausts blasting operation) was 1.78 g/d. Again, a day represents six hours of operation over a 24-hour period.

III. CONCLUSION

Based on the results of this survey, the beryllium emissions from the brake reconditioning operation are well below the EPA standards established in 40 CFR 61.30 of 10 g/d.

TABLE 1: SURVEY EMISSION RESULTS

<u>Sample Site</u>	<u>Sample Date</u>	<u>Probe Location (%) (% Duct Diameter)</u>	<u>% of iso-kinetic Sampling</u>	<u>Emission Rate (g/d)</u>	<u>Avg Emission Rate (g/d)</u>
East					
Run 1	17 Jul	25	99.9	<0.027	<0.028
	17 Jul	50	93.8	<0.029	
	17 Jul	75	93.1	<0.029	
West					
Run 1	15 Jul	25	96.3	0.76	1.78
	16 Jul	75	107.0	1.25	
	16 Jul	50	93.1	3.28	

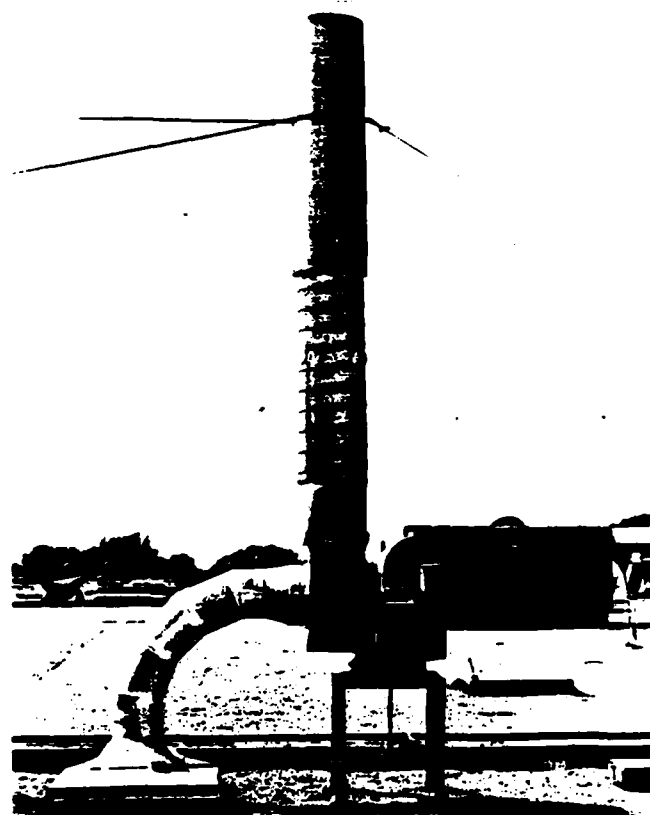


FIGURE 1: Sampling Site on the Roof

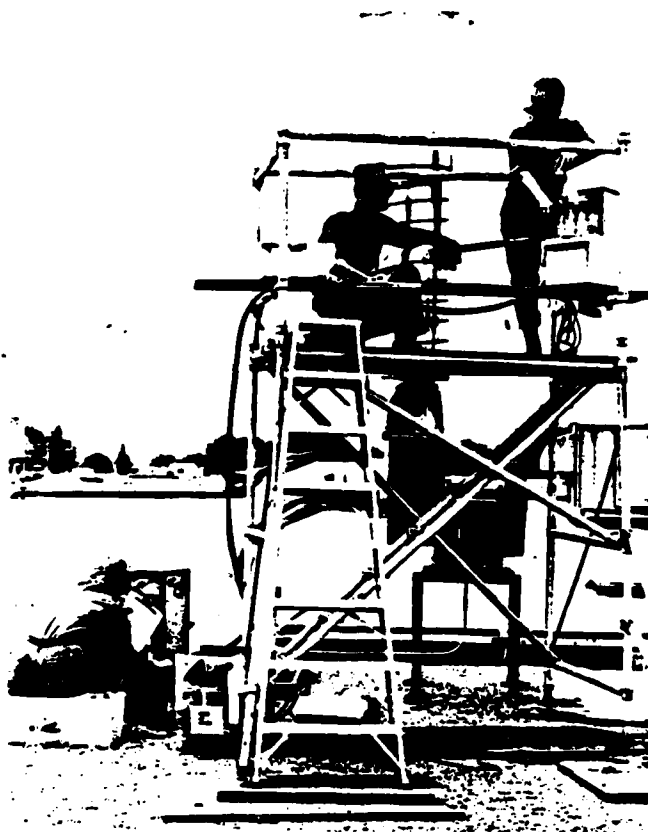


FIGURE 2: Sampling Equipment and Personnel

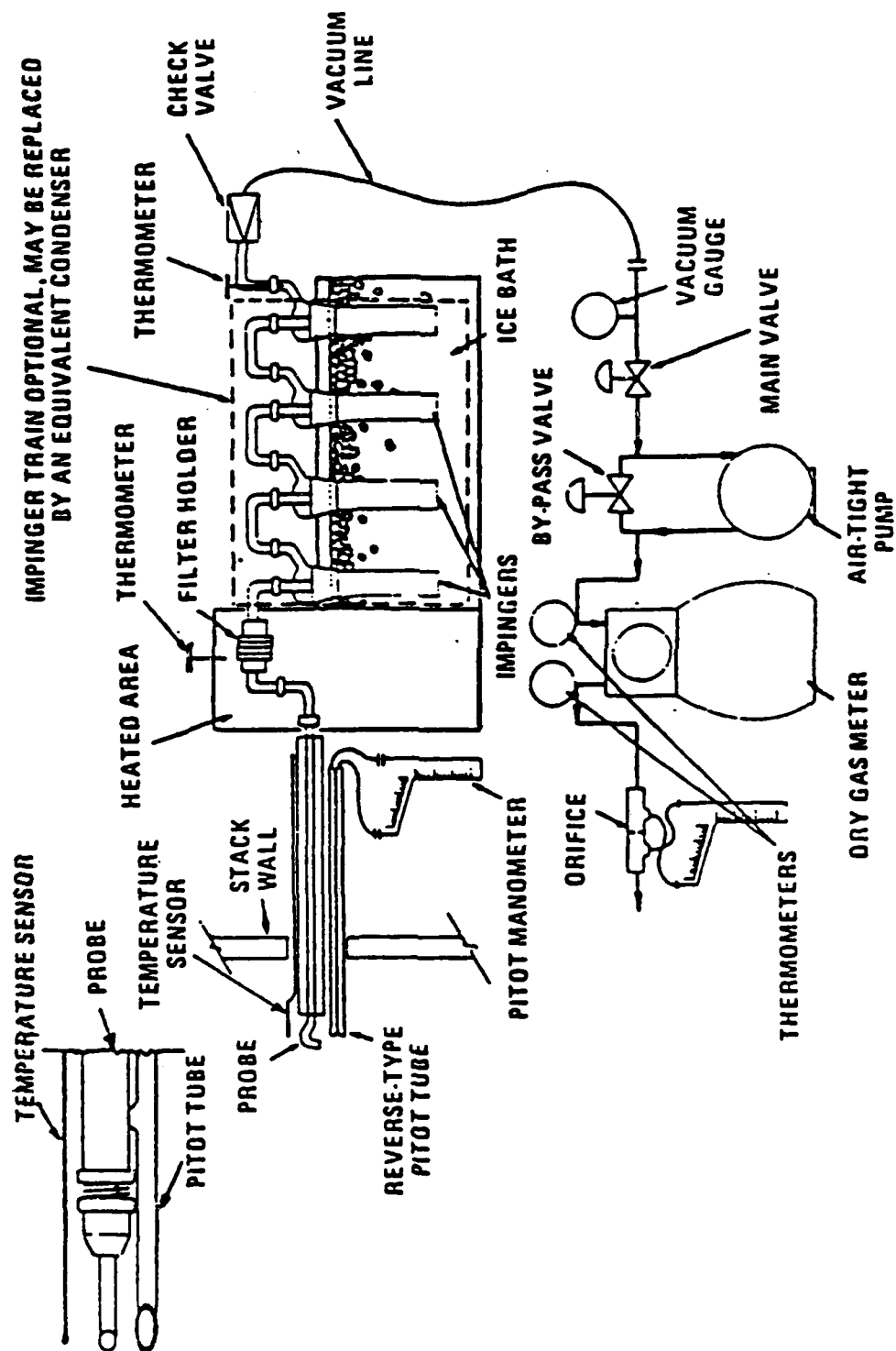


FIGURE 3: Method 5 Sampling Train

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Appendix A
TEST PARTICIPANTS

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TEST PARTICIPANTS

1. USAFOEHL/ECQ Sampling Team
Brooks AFB TX 78235-5501
(512) 536-2891

Maj James Garrison
Capt Guy Fagin
Capt Mary Daly
A1C Donald Johnson

2. Personnel Contacted

Lt Col Phillip Brown, USAF Hosp Hill/SGPB
Mr Willert Farrell, USAF Hosp Hill/SGPB
Mr Dick Stiefkin, USAF Hosp Hill/SGPB
Mr Robert Berger, OO-ALC/MANPGW

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Appendix B
SURVEY RAW DATA - East Stack

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PRELIMINARY SURVEY DATA SHEET NO. 2
(Velocity and Temperature Traversal)

BASE <u>Kii</u>	DATE <u>17 July</u>
BOILER NUMBER <u>East</u>	
INSIDE STACK DIAMETER <u>15.75</u> Inches	
STATION PRESSURE	
STACK STATIC PRESSURE <u>East</u> <u>+ 0.07</u> In Hg	
SAMPLING TEAM	

TRAVERSE POINT NUMBER	VELOCITY HEAD V_p IN H ₂ O <u>Port A</u>	$\sqrt{V_p}$ <u>Port B</u>	STACK TEMPERATURE (°F)
1	0.11	0.015	
2	0.11	0.015	
3	0.10	0.055	
4	0.095	0.065	
5	0.08 / 0.075	0.085	
6	0.085	0.11	
7	0.185	0.20	
8	0.205	0.22	
9	0.205	0.225	
10	.195	0.225	
11	.175	0.215	
12	.175	0.215	
50%	0.13	0.16	
C = 1.15			
T _a = 80 / 63			
W			
-1.5 in H ₂ O	.369 / 369 / 368		
1.5 in H ₂ O	.372		
1.5 in H ₂ O	.023 AVERAGE		

PARTICULATE SAMPLING DATA SHEET

RUN NUMBER Run 1		SCHEMATIC OF STACK CROSS SECTION @ 25% stack 120 min leak zero/min @ 5"		EQUATIONS $OR = OF + 460$ $H = \left[\frac{5130 \cdot P \cdot C_p \cdot A}{C_o} \right]^2 \cdot \frac{T_m}{T_o} \cdot V_p$		AMBIENT TEMP STATION PRESS 24.92 HEATER BOX TEMP OF PROBE HEATER SETTING OF PROBE LENGTH in NOZZLE AREA (A) 0.35 sq ft DRY GAS FRACTION (F _D)	
DATE 17 July 87		PLANT east Be		METER BOX NUMBER 11111513		STOP 124.797 Start 42.416	

TRAVERSE POINT NUMBER	SAMPLING TIME (min)	STATIC PRESSURE (in H ₂ O)	STACK TEMP		VELOCITY HEAD (Vp)	ORIFICE DIFF. PRESS. (H)	GAS SAMPLE VOLUME (cu ft)	GAS METER TEMP			SAMPLE BOX TEMP (OF)	IMPINGER OUTLET TEMP (OF)
			(OF)	(T _s) (OR)				IN (OF)	AVG (T _m) (OR)	OUT (OF)		
1	1820	0.074	71		0.075	1.7	42.416	65	65.5	64	233	70
2	0825		71		0.075	1.7	45.7	66	65	64	231	70
3	0830		70		0.08	1.8	49.1	68	66.5	65	232	70
4	0835		70		0.075	1.7	52.1	69	67	65	240	70
5	0840		71		0.075	1.7	56.0	71	68.5	66	246	70
6	0845		71		0.075	1.7	59.4	73	70	67	248	70
7	0850		73		0.075	1.7	62.9	75	71.5	68	256	70
8	0855		73		0.075	1.7	66.3	76	72.5	69	262	70
9	0900		73		0.075	1.7	70.0	77	73.5	70	263	70
10	0905		74		0.075	1.7	73.2	78	74.5	71	254	70
11	0910		74		0.075	1.7	76.6	79	75	71	254	70
12	0915		74		0.075	1.7	80.0	79	75.5	72	261	70
13	0920		74		0.075	1.7	83.4	80	76.5	73	267	70
14	0925		74		0.075	1.7	86.85	80	76.5	73	261	70
15	0930		74		0.075	1.7	90.3	81	77.5	74	261	70
16	0935		75		0.075	1.7	93.8	82	78.5	75	242	70
17	0940		75		0.075	1.7	97.2	82	78.5	75	243	70
18	0945		75		0.075	1.7	100.6	83	79.5	76	243	70
19	0950		76		0.075	1.7	104.1	84	80	76	244	70
20	0955		76		0.075	1.7	107.5	84	80.5	77	247	70
21	1000		77		0.075	1.7	111.0	84	80.5	77	247	70
22	1005		78		0.075	1.7	114.4	85	81.5	78	243	70
23	1010		76		0.075	1.7	117.9	85	81.5	78	241	70
OEH			4	77	0.075	1.7	121.3	86	82.5	79	241	70

PARTICULATE SAMPLING DATA SHEET

RUN NUMBER		SCHEMATIC OF STACK CROSS SECTION		EQUATIONS		AMBIENT TEMP						
DATE	PLANT	BASE	SAMPLE BOX NUMBER	METER BOX NUMBER	Q _m /Q _m	C _o	OF					
2	17 July 87	east R.C.	Hill AFB				STATION PRESS 24.90					
							HEATER BOX TEMP					
							PROBE HEATER SETTING					
							PROBE LENGTH					
							NOZZLE AREA (A)					
							C _p					
							DRY GAS FRACTION (F _d)					
		at 50% traverse 120 mm wake @ 6" Hg zero leak		$H = \left[\frac{5130 \cdot F_d \cdot C_p \cdot A}{C_o} \right]^2 \cdot \frac{T_m \cdot V_p}{T_s}$								
		Stop 220.796 Start 124.956										
TRAVERSE POINT NUMBER	SAMPLING TIME (min)	STATIC PRESSURE (in H ₂ O)	STACK TEMP (°F)	STACK TEMP (T _s) (°F)	VELOCITY HEAD (V _p)	ORIFICE DIFF. PRESS. (in)	GAS SAMPLE VOLUME (cu ft)	GAS METER TEMP IN (°F)	GAS METER TEMP AVG (T _m) (°F)	GAS METER TEMP OUT (°F)	SAMPLE BOX TEMP (°F)	IMPINGER OUTLET TEMP (°F)
1	10:50	0.07	87		.105	2.3	124.956	78	77.5	77	827	76
2	10:55		87		.11	2.3	124.956	81	78.5	78	237	76
3	11:00		88		.11	2.3	132.7	82	80	79	243	70
4	11:05		88		.11	2.3	126.7	84	81	78	236	70
5	11:10		88		.11	2.3	130.7	87	81.5	79	247	70
6	11:15		88		.115	2.6	174.7	87	82	79	230	70
7	11:20		88		.11	2.3	179.6	88	83	80	251	70
8	11:25		88		.11	2.3	152.6	87	83.5	80	236	70
9	11:30		88		.11	2.3	156.6	87	83.5	80	218	70
10	11:35		88		.11	2.3	160.6	88	84.5	81	259	70
11	11:40		88		.115	2.6	164.4	88	85	82	297	70
12	11:45		88		.115	2.6	168.4	89	86	83	243	70
13	11:50		88		.115	2.6	172.4	89	86	83	246	70
14	11:55		88		.115	2.6	176.4	90	87	84	292	70
15	12:00		88		.115	2.6	180.4	91	87.5	84	250	70
16	12:05		88		.115	2.6	184.4	92	88.5	85	278	70
17	12:10		88		.12	2.7	188.4	92	89	86	242	70
18	12:15		88		.12	2.7	192.4	93	89.5	86	243	70
19	12:20		88		.11	2.5	196.4	93	90	87	240	70
20	12:25		88		.11	2.5	200.4	93	90	87	248	70
21	12:30		88		.11	2.5	204.4	93	90	87	249	70
22	12:35		88		.115	2.6	208.4	93	90	87	247	70
23	12:40		88		.115	2.6	212.4	94	91	88	247	70
24	12:45		88		.11	2.5	216.4	94	91	88	245	70

OEH FORM 18 MAY 76

PARTICULATE SAMPLING DATA SHEET

RUN NUMBER 3		SCHEMATIC OF STACK CROSS SECTION 75% clean velocity		EQUATIONS $H = \left[\frac{5130 \cdot F \cdot G \cdot A}{C_0} \right]^2 \cdot \frac{T_m \cdot V_p}{T_0}$		AMBIENT TEMP 24.87	
DATE 17 JUL 81		120 mm				STATION PRESS 24.87	
PLANT East						HEATER BOX TEMP	
BASE H.00 AFB		leak 10" Hg zero leak/min				PROBE HEATER SETTING	
SAMPLE BOX NUMBER						PROBE LENGTH	
METER BOX NUMBER						NOZZLE AREA (A) 1.37	
Q _w /Q _m						C _p	
C ₀						DRY GAS FRACTION (F _d)	

ref ΔP = 0.085

stop 360.591
start 221.042

TRAVERSE POINT NUMBER	SAMPLING TIME (min)	STATIC PRESSURE (in H ₂ O)	STACK TEMP (°F) (T ₀)	VELOCITY HEAD (V _p)	ORIFICE DIFF. PRESS. (H)	GAS SAMPLE VOLUME (cu ft)	GAS METER TEMP (°F) (T _m)	SAMPLE BOX TEMP (°F)	IMPINGING OUTLET TEMP (°F)
1	1320	0.07	86	0.21	4.1	221.042	89	226	70
2	1325		88	0.235	4.65	221.1	92	250	70
3	1330		86	0.23	4.8	213.7	96	268	70
4	1335		88	0.23	4.8	237.4	97	266	70
5	1340		88	0.235	4.9	243.2	98	252	70
6	1345		94	0.235	4.9	248.9	98	261	70
7	1350		96	0.23	4.8	254.7	100	237	70
8	1355		98	0.23	4.9	260.5	100	250	70
9	1400		93	0.235	4.9	266.2	99	257	70
10	1405		86	0.24	5.0	272.0	99	261	70
11	1410		77	0.24	5.0	277.8	99	256	70
12	1415		77	0.24	5.0	283.7	100	250	70
13	1420		93	0.24	5.0	289.5	101	247	70
14	1425		91	0.245	5.2	295.4	101	247	70
15	1430		91	0.245	5.2	301.3	103	248	70
16	1435		91	0.24	5.0	307.3	104	247	70
17	1440		97	0.24	5.0	313.2	104	247	70
18	1445		97	0.24	5.0	319.3	104	248	70
19	1450		91	0.24	5.0	325.1	104	248	70
20	1455		97	0.245	5.2	331.0	105	245	70
21	1500		92	0.245	5.2	336.9	104	247	70
22	1505		93	0.245	5.2	342.9	104	247	70
23	1510		95	0.24	5.0	348.8	105	246	70
TOTAL		10	97	0.24	5.0	354.7	106	248	70

AIR POLLUTION PARTICULATE ANALYTICAL DATA

BASE <i>Hill</i>		DATE <i>17 July</i>		RUN NUMBER <i>I</i>	
BUILDING NUMBER <i>East Be</i>			SOURCE NUMBER <i>East Be</i>		
I. PARTICULATES					
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT PARTICLES (gm)		
FILTER NUMBER <i>millipore 5</i> <i>11741 12</i>					
ACETONE WASHINGS (Probe, Front Half Filter)					
BACK HALF (if needed)					
		Total Weight of Particulates Collected			
II. WATER					
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT WATER (gm)		
IMPINGER 1 (H2O)	<i>87</i>	<i>100</i>	<i>—</i>		
IMPINGER 2 (H2O)	<i>106</i>	<i>100</i>	<i>6</i>		
IMPINGER 3 (Dry)	<i>5</i>	<i>0</i>	<i>5</i>		
IMPINGER 4 (Silica Gel)	<i>226.17</i> <i>20</i>	<i>200.55</i>	<i>25.62</i>		
		Total Weight of Water Collected			
		<i>424.17</i>	<i>400.55</i>	<i>23.62</i> <i>36.62</i>	
III. GASES (Dry)					
ITEM	ANALYSIS 1	ANALYSIS 2	ANALYSIS 3	ANALYSIS 4	AVERAGE
VOL % CO ₂					
VOL % O ₂					
VOL % CO					
VOL % N ₂					
Vol % N ₂ = (100% - % CO ₂ - % O ₂ - % CO)					

AIR POLLUTION PARTICULATE ANALYTICAL DATA

BASE <i>Hill</i>	DATE <i>17 July 87</i>	RUN NUMBER <i>Run II</i>
---------------------	---------------------------	-----------------------------

BUILDING NUMBER <i>East Be</i>	SOURCE NUMBER
-----------------------------------	---------------

I. PARTICULATES			
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT PARTICLES (gm)
FILTER NUMBER <i>mill 6</i> <i>W 41 13</i>			
ACETONE WASHINGS (Probe, Front Half Filter)			
BACK HALF (If needed)			
Total Weight of Particulates Collected			

II. WATER			
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT WATER (gm)
IMPINGER 1 (H2O)	<i>83</i> <i>87</i>	<i>100</i>	<i>0</i>
IMPINGER 2 (H2O)	<i>108</i> <i>106</i>	<i>100</i>	<i>8</i>
IMPINGER 3 (Dry)	<i>2</i> <i>5</i>	<i>0</i>	<i>2</i>
IMPINGER 4 (Silica Gel)	<i>227.92</i> <i>226.17</i>	<i>202.35</i>	<i>25.57</i>
Total Weight of Water Collected <i>420.92 - 402.35</i>			<i>18.57</i> <i>35.57</i>

III. GASES (Dry)					
ITEM	ANALYSIS 1	ANALYSIS 2	ANALYSIS 3	ANALYSIS 4	AVERAGE
VOL % CO ₂					
VOL % O ₂					
VOL % CO					
VOL % N ₂			<i>733</i>	<i>671</i>	<i>imp + 5.9</i>

<i>Unsat = H₂O</i> <i>77 + 44</i>	Vol % N ₂ = (100% - % CO ₂ - % O ₂ - % CO)	<i>487 imp</i>
---	---	----------------

AIR POLLUTION PARTICULATE ANALYTICAL DATA

BASE <i>H111</i>	DATE <i>17 July</i>	RUN NUMBER <i>3</i>
---------------------	------------------------	------------------------

BUILDING NUMBER <i>East Be</i>	SOURCE NUMBER
-----------------------------------	---------------

I. PARTICULATES			
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT PARTICLES (gm)
FILTER NUMBER <i>m w41</i>	<i>7 14</i>		
ACETONE WASHINGS (Probe, Front Half Filter)			
BACK HALF (if needed)			
	Total Weight of Particulates Collected		gm

II. WATER			
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT WATER (gm)
IMPINGER 1 (H ₂ O)	<i>87</i> 62	<i>100</i>	<i>0</i>
IMPINGER 2 (H ₂ O)	<i>100</i>	<i>100</i>	<i>0</i>
IMPINGER 3 (Dry)	<i>6</i>	<i>0</i>	<i>6</i>
IMPINGER 4 (Silica Gel)	<i>235.00</i>	<i>202.29</i>	<i>32.71</i>
	<i>428</i> Total Weight of Water Collected		<i>42.29</i> <i>25.71</i>

III. GASES (Dry)					
ITEM	ANALYSIS 1	ANALYSIS 2	ANALYSIS 3	ANALYSIS 4	AVERAGE
VOL % CO ₂					
VOL % O ₂					
VOL % CO					
VOL % N ₂					

mnsc 88112
H₂O

$$\text{Vol \% N}_2 = (100\% - \% \text{CO}_2 - \% \text{O}_2 - \% \text{CO})$$

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Appendix C
SURVEY RAW DATA - West Stack

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PRELIMINARY SURVEY DATA SHEET NO. 1
(Stack Geometry)

BASE <i>Hill</i>	PLANT <i>Black Spruce</i>
DATE <i>15 Dec 87</i>	SAMPLING TEAM
SOURCE TYPE AND MAKE	
SOURCE NUMBER <i>Stack 1</i>	INSIDE STACK DIAMETER <i>15.75"</i> Inches
RELATED CAPACITY	TYPE FUEL
DISTANCE FROM OUTSIDE OF NIPPLE TO INSIDE DIAMETER <i>15 3/4"</i> Inches	
NUMBER OF TRAVERSES	NUMBER OF POINTS/TRAVERSE

LOCATION OF SAMPLING POINTS ALONG TRAVERSE

POINT	PERCENT OF DIAMETER	DISTANCE FROM INSIDE WALL <i>TRAVEL</i> (Inches) <i>3</i>	TOTAL DISTANCE FROM OUTSIDE OF NIPPLE TO SAMPLING POINT (Inches)
<i>1</i>	<i>2.1</i>		<i>1"</i>
<i>2</i>	<i>6.7</i>		<i>1"</i>
<i>3</i>	<i>11.8</i>		<i>1.9</i>
<i>4</i>	<i>17.7</i>		<i>2.8</i>
<i>5</i>	<i>25.0</i>		<i>3.9</i> *
<i>6</i>	<i>35.6</i>		<i>5.6</i>
<i>7</i>	<i>54.4</i>		<i>10</i>
<i>8</i>	<i>75.0</i>		<i>11.8</i> *
<i>9</i>	<i>82.3</i>		<i>13</i>
<i>10</i>	<i>88.2</i>		<i>13.9</i>
<i>11</i>	<i>93.3</i>		<i>14.75</i>
<i>12</i>	<i>97.9</i>		<i>15 → 14.75</i>
	<i>50.0</i>		<i>29</i> *

PRELIMINARY SURVEY DATA SHEET NO. 2
(Velocity and Temperature Traverse)

BASE

4/1/11

DATE _____

15 July 87

BOILER NUMBER

West

INSIDE STACK DIAMETER

15.75"

Inches

STATION PRESSURE

La Hg

STACK STATIC PRESSURE

$$+ 0.04 \frac{\rho_{\text{ort}}}{A} / 0.04 \frac{\rho_{\text{ort}}}{B}$$

Ln H2O

SAMPLING TEAM

TRAVERSE POINT NUMBER	VELOCITY HEAD, V_p IN H ₂ O	Part $\sqrt{V_p}$ B	STACK TEMPERATURE (°F)
1	0.02	0.035	
2	0.02	0.035	
3	0.025	0.045	
4	0.03	0.045	
5 *	0.03	0.055	
6	0.04	0.070	
7	0.10	0.125	
8	0.11	0.13	
9	0.10	0.13	
10	0.095	0.125	
11	0.085	0.125	
12	0.085	0.125	
	$AH @ = 2.13$		
	$T_m = 84^\circ F$		
	$w \Delta p = 0.03$		
	$C = 1.2$		
	$T_s = 80$		
d	$80/59$		
	w		
	total normal	0.475	
	AVERAGE normal	0.	

PRELIMINARY SURVEY DATA SHEET NO. 2
(Velocity and Temperature Traverses)

BASE

Hill BEB

JAYC

16 July 8' (1200)

BOILER NUMBER

Wast 30

INSIDE STACK DIAMETER

Inches

STATION PRESSURE

En 11g

STACK STATIC PRESSURE

Ln H2O

SAMPLING TEAM

TRAVERSE POINT NUMBER	VELOCITY HEAD, v_p IN H ₂ O	$\sqrt{v_p}$	STACK TEMPERATURE (°F)
1	0.025		
2	0.025		
3	0.025		
4	0.030		
5	0.035		
6	0.045		
7	0.075		
8	0.065		
9	0.060		
10	0.060		
11	0.055		
12	0.055		
50%	0.065		
AVERAGE			

PARTICULATE SAMPLING DATA SHEET									
SCHEMATIC OF STACK CROSS SECTION				EQUATIONS				AMBIENT TEMP	
TRaverse POINT NUMBER	SAMPLING TIME (min)	STATIC PRESSURE (in H ₂ O)	STACK TEMP (°F)	VELOCITY HEAD (Vp)	ORIFICE DIFF. PRESS. (in)	GAS SAMPLE VOLUME (cu ft)	GAS METER TEMP (°F)	SAMPLE BOX TEMP (°F)	IMPINGER OUTLET TEMP (°F)
1	1200	0.0415	97	0.035	2.65	777.010	104	239	70
2	1205	17	97	0.035	2.65	781.2	103	250	70
3	1210	7	90	0.035	2.65	785.5	106	252	70
4	1215	7	82	0.035	2.65	789.8	109	252	70
5	1220	5	79	0.035	2.65	794.1	112	253	70
6	1225	7	82	0.035	2.65	798.45	114	249	70
7	1230	7	77	0.035	2.65	802.2	116	249	70
8	1235	7	75	0.035	2.65	807.2	118	251	70
9	1240	7	74	0.035	2.65	811.5	119	256	70
10	1245	7	77	0.035	2.65	815.9	120	252	70
11	1250	6	74	0.030	2.3	820.3	121	250	70
12	1255	7	74	0.035	2.65	824.5	121	245	70
13	1300	6	71	0.030	2.3	828.5	122	251	70
14	1305	6	73	0.030	2.3	833.0	122	246	70
15	1310	6	78	0.030	2.3	837.0	123	245	70
16	1315	6	82	0.030	2.3	841.1	124	250	70
17	1320	6	82	0.030	2.3	845.2	124	250	70
18	1325	6	81	0.030	2.3	849.3	125	250	70
19	1330	6	72	0.030	2.3	853.4	125	244	70
20	1335	6	69	0.030	2.3	857.45	125	243	70
21	1340	6	69	0.035	2.65	861.5	126	256	70
22	1345	6	70	0.030	2.3	865.3	126	254	70
23	1350	6	67	0.030	2.3	869.4	127	258	70
TOTAL				0.035	2.65	873.4	127	247	70

FORM 18
MAY 78

PARTICULATE SAMPLING DATA SHEET

RUN NUMBER <u>2</u>		SCHEMATIC OF STACK CROSS SECTION		EQUATIONS		AMBIENT TEMP	
DATE <u>16 July 87</u>		<p>at .75 Traversal pt</p> <p>zero leak/min</p> <p>stop 922.392</p> <p>Start 878.051</p>		°R = °F + 460		STATION PRESS	
PLANT <u>West Be</u>				$H = \left[\frac{5130 \cdot F \cdot C \cdot A}{C_o} \right]^2 \cdot \frac{T_m \cdot V_p}{T_o}$		HEATER BOX TEMP	
BASE <u>Hill Hill</u>						PROBE HEATER SETTING	
SAMPLE BOX NUMBER <u>1 ac</u>						PROBE LENGTH	
METER BOX NUMBER <u>nutack</u>						NOZZLE AREA (A)	
Qm/Qm				sq ft			
Co				DRY GAS FRACTION (F _d)			

TRAVERSE POINT NUMBER	SAMPLING TIME (min)	STATIC PRESSURE (in H ₂ O)	STACK TEMP		VELOCITY HEAD (Vp)	ORIFICE DIFF. PRESS. (in)	GAS SAMPLE VOLUME (cu ft)	GAS METER TEMP			SAMPLE BOX TEMP (°F)	IMPINGER OUTLET TEMP (°F)
			(°F)	(T _o) (°R)				IN (°F)	AVG (T _m) (°R)	OUT (°F)		
1	0730	0.04	82		.04	.4	878.05	74	73	72	232	70
2	0735		82		.045	.45	879.8	74	73	72	245	70
3	0740		80		.05	.5	881.6	75	74	74	250	70
4	0745		78		.045	.45	883.5	77	77	75	248	70
5	0750		80		.043	.3	885.35	81	78.5	76	251	70
6	0755		83		.045	.45	886.9	83	80	77	253	70
7	0800		83		.05	.5	888.6	85	82	79	258	70
8	0805		82		.05	.5	890.5	86	83	80	247	70
9	0810		85		.05	.5	893	89	85.5	82	244	70
10	0815		89		.05	.5	894.4	90	86.5	83	246	70
11	0820		90		.035	.35	896.4	92	88.5	85	244	70
12	0825		91		.035	.35	898.1	93	88.5	86	243	70
13	0830		90		.045	.45	899.9	94	90.5	87	244	70
14	0835		87		.05	.5	902.0	95	92	89	241	70
15	0840		88		.045	.45	903.7	96	93	90	241	70
16	0845		87		.045	.45	905.6	97	93.5	90	242	70
17	0850		88		.035	.35	907.5	98	95	92	240	70
18	0855		89		.045	.45	909.2	98	95	92	248	70
19	0900		84		.045	.45	911.9	98	95.5	93	250	70
20	0905		88		.045	.45	913.9	99	96.5	94	248	70
21	0910		89		.045	.45	914.8	100	97.5	95	250	70
22	0915		91		.045	.45	916.7	100	98	96	246	70
23	0920		89		.035	.35	918.6	100	98	96	248	70
OEHL FORM 18 MAY 78			5/4 89		.035	.35	920.3	101	98.5	96	249	70

PARTICULATE SAMPLING DATA SHEET												
SCHEMATIC OF STACK CROSS SECTION				EQUATIONS								
RUN NUMBER	DATE	PLANT	BASE	SAMPLE BOX NUMBER	METER BOX NUMBER	Qw/Qm	Co	$H = \left[\frac{5130 \cdot P \cdot C_p \cdot A}{C_o} \right]^2 \cdot \frac{T_m \cdot V_p}{T_o}$ $R = 0^\circ F + 460$		AMBIENT TEMP		
								STATION PRESS	OF			
								HEATER BOX TEMP	In Hg			
								PROBE HEATER SETTING	OF			
								PROBE LENGTH	IN			
								NOZZLE AREA (A)	sq ft			
								DRY GAS FRACTION (Fd)				
@ 50% traverse 115 mm turn 1205 → 1400 leak 0 in mm @ 11" vac Stop 1041.718 Start 923.143								$d = 0.5$ $W/LP = 0.025$				
TRAVERSE POINT NUMBER	SAMPLING TIME (min)	STATIC PRESSURE (in H2O)	STACK TEMP (°F)	STACK TEMP (°R)	VELOCITY HEAD (Vp)	GAUGE DIFF. PRESS. (H)	GAS SAMPLE VOLUME (cu ft)	GAS METER TEMP IN (°F)	GAS METER TEMP AVG (°R)	GAS METER TEMP OUT (°F)	SAMPLE BOX TEMP (°F)	IMPINGER OUTLET TEMP (°F)
1	1205	0.04	84		0.075	5.3	923.143	101	100	99	243	70
2	1210		85		0.075	5.3		101	100	99	243	70
3	1215		86		0.075	5.3	934.7	103	101	99	246	70
4	1220		83		0.035	2.6	940.6	105	102	100	244	70
5	1225		82		0.035	2.6	945.0	105	102	100	248	70
6	1230		84		0.065	4.7	949.3	107	103	100	246	70
7	1235		82		0.065	4.7	954.9	110	106	102	247	70
8	1240		85		0.065	4.7	960.7	111	107	103	247	70
9	1245		83		0.065	4.7	966.3	112	108	103	248	70
10	1250		89		0.035	2.6	972.0	112	108	104	247	70
11	1255		89		0.035	2.6	976.4	112	108	104	248	70
12	1300		76		0.05	3.6	980.7	114	110	106	248	70
13	1305		79		0.05	3.6	985.7	116	111	107	251	70
14	1310		83		0.05	3.6	990.7	118	115	107	251	70
15	1315		92		0.05	3.6	995.8	118	112	108	253	70
16	1320		83		0.035	2.6	1001.8	117	113	109	253	70
17	1325		87		0.035	2.6	1005.5	117	113	110	253	70
18	1330		97		0.055	4.0	1009.5	118	114	110	245	70
19	1335		97		0.055	4.0	1014.8	118	114	110	245	70
20	1340		97		0.065	4.7	1020.0	118	114	111	245	70
21	1345		117		0.065	4.7	1025.9	118	115	112	247	70
22	1350		117		0.05	3.6	1031.6	118	115	112	245	70
23	1355		119		0.05	3.6	1036.6	118	114	111	245	70

AIR POLLUTION PARTICULATE ANALYTICAL DATA

BASE <i>Hill</i>		DATE <i>15 July</i>		RUN NUMBER <i>I West Stack</i>	
BUILDING NUMBER <i>West</i>			SOURCE NUMBER <i>Be</i>		
I. PARTICULATES					
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT PARTICLES (gm)		
FILTER NUMBER <i>1</i>	<i>.2775</i>	<i>0.2715</i>			
ACETONE WASHINGS (Probe, Front Half Filter)					
BACK HALF (if needed)					
		Total Weight of Particulates Collected			
II. WATER					
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT WATER (gm)		
IMPINGER 1 (N2O)	<i>91</i>	<i>100</i>	<i>-9</i>		
IMPINGER 2 (N2O)	<i>106</i>	<i>100</i>	<i>6</i>		
IMPINGER 3 (Dry)	<i>5</i>	<i>0</i>	<i>5</i>		
IMPINGER 4 (Silica Gel)	<i>228.48</i>	<i>201.72</i>	<i>26.76</i>		
		Total Weight of Water Collected <i>430.48 - 401.72</i>		<i>28.76 -</i>	
III. GASES (Dry)					
ITEM	ANALYSIS 1	ANALYSIS 2	ANALYSIS 3	ANALYSIS 4	AVERAGE
VOL % CO ₂					
VOL % O ₂					
VOL % CO					
VOL % N ₂					
<i>moist H₂O 121 ml</i> <i>gas sample</i> $\text{Vol \% N}_2 = (100\% - \% \text{CO}_2 - \% \text{O}_2 - \% \text{CO})$					

AIR POLLUTION PARTICULATE ANALYTICAL DATA

BASE <i>Hill</i>	DATE <i>16 July</i>	RUN NUMBER <i>II</i>
BUILDING NUMBER <i>West</i>	SOURCE NUMBER <i>BE</i>	

I. PARTICULATES			
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT PARTICLES (gm)
FILTER NUMBER <i>2</i> <i>10</i>	<i>.2824</i>	<i>.2730</i>	
ACETONE WASHINGS (Probe, Front Half Filter)			
BACK HALF (If needed)			
	Total Weight of Particulates Collected		

II. WATER			
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT WATER (gm)
IMPINGER 1 (H2O)	<i>106</i>	<i>100</i>	<i>6</i>
IMPINGER 2 (H2O)	<i>104</i>	<i>100</i>	<i>4</i>
IMPINGER 3 (Dry)	<i>1</i>	<i>∅</i>	<i>1</i>
IMPINGER 4 (Silica Gel)	<i>212.05</i>	<i>201.36</i>	<i>10.69</i>
	Total Weight of Water Collected <i>423.05 - 401.36</i>		<i>21.69 -</i>

III. GASES (Dry)					
ITEM	ANALYSIS 1	ANALYSIS 2	ANALYSIS 3	ANALYSIS 4	AVERAGE
VOL % CO ₂					
VOL % O ₂					
VOL % CO					
VOL % N ₂					

revised glassware *141* Vol % N₂ = (100% - % CO₂ - % O₂ - % CO)

AIR POLLUTION PARTICULATE ANALYTICAL DATA

BASE <div style="font-size: 1.5em; font-family: cursive;">H111</div>	DATE <div style="font-size: 1.5em; font-family: cursive;">16 July</div>	RUN NUMBER <div style="font-size: 1.5em; font-family: cursive;">3</div>
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BUILDING NUMBER <div style="font-size: 1.5em; font-family: cursive;">West Be</div>	SOURCE NUMBER
--	--------------------------

I. PARTICULATES			
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT PARTICLES (gm)
FILTER NUMBER <div style="font-size: 1.2em; font-family: cursive;">millipore What 41</div>	<div style="font-size: 1.2em; font-family: cursive;">4.2758</div> <div style="font-size: 1.2em; font-family: cursive;">11</div>	<div style="font-size: 1.2em; font-family: cursive;">.2743</div>	
ACETONE WASHINGS (Probe, Front Half Filter)			
BACK HALF (if needed)			
	Total Weight of Particulates Collected		-

II. WATER			
ITEM	FINAL WEIGHT (gm)	INITIAL WEIGHT (gm)	WEIGHT WATER (gm)
IMPINGER 1 (H2O)	<div style="font-size: 1.5em; font-family: cursive;">87</div>	<div style="font-size: 1.5em; font-family: cursive;">100</div>	<div style="font-size: 1.5em; font-family: cursive;">0</div>
IMPINGER 2 (H2O)	<div style="font-size: 1.5em; font-family: cursive;">108</div>	<div style="font-size: 1.5em; font-family: cursive;">100</div>	<div style="font-size: 1.5em; font-family: cursive;">8</div>
IMPINGER 3 (Dry)	<div style="font-size: 1.5em; font-family: cursive;">6</div>	<div style="font-size: 1.5em; font-family: cursive;">Ø</div>	<div style="font-size: 1.5em; font-family: cursive;">6</div>
IMPINGER 4 (Silica Gel)	<div style="font-size: 1.5em; font-family: cursive;">231.85</div>	<div style="font-size: 1.5em; font-family: cursive;">205.02</div>	<div style="font-size: 1.5em; font-family: cursive;">26.83</div>
	<div style="font-size: 1.2em; font-family: cursive;">432.85</div>	<div style="font-size: 1.2em; font-family: cursive;">405.02</div>	<div style="font-size: 1.2em; font-family: cursive;">27.83</div>
	Total Weight of Water Collected		<div style="font-size: 1.5em; font-family: cursive;">40.83</div>

III. GASES (Dry)					
ITEM	ANALYSIS 1	ANALYSIS 2	ANALYSIS 3	ANALYSIS 4	AVERAGE
VOL % CO ₂					
VOL % O ₂					
VOL % CO					
VOL % N ₂					

Method 121
 S. G. W. H. T. R.

$$\text{Vol \% N}_2 = (100\% - \% \text{CO}_2 - \% \text{O}_2 - \% \text{CO})$$

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Appendix D

QUALITY ASSURANCE - CALIBRATION DATA

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ANALYTICAL BALANCE CALIBRATION FORM

Balance name Mettler PC440 Number —

Classification of standard weights S class

Date	0.500 g	1.0000 g	10.0000 g	50.0000 g	100.0000 g	Analyst
16 July	.50	1.00	10.00	50.00	100.00	MD
17 July	.50	1.00	10.00	50.00	100.00	MD

Quality Assurance Handbook M5-5.2

METER BOX CALIBRATION DATA AND CALCULATION FORM

(English units)

Date 17 Mar 87

Meter box number Nutech

Barometric pressure, $P_b = 28.941$ in. Hg

Calibrated by Moran + Daly

Orifice manometer setting (ΔH), in. H ₂ O	Gas volume		Temperature				Time (θ), min	Y_i	$\Delta H \theta_i$ in. H ₂ O
	Wet test meter (V_w), ft ³	Dry gas meter (V_d), ft ³	Wet test meter (t_w), °F	Dry gas meter					
				Inlet (t_{d_i}), °F	Outlet (t_{d_o}), °F	Avg ^a (t_d), °F			
0.5	4.651 5	49.533 44.882	69.4 68.9529.1	77 73	72 70	533	13.5	1.08	2.10
1.0	4.658 5	55.036 50.378	70.3 69.1529.7	82 78	74 72	536.5	9.6	1.08	2.11
1.5	7.370 7	65.254 55.882	68.9 70.7529.8	88 83	78 75	541	15.8	1.085	2.13
2.0	9.405 7	75.417 66.012	67.8 69.4528.6	93 89	82 79	545.75	13.8	1.09	2.14
3.0	9.427 10	85.799 76.372	70.3 68.2529.3	98 94	85 83	550	11.3	1.09	2.14
4.0	9.251 10	95.753 99.502	68.5 68.5528.5	80 75	71 70	534	9.75	1.08	2.18
Avg								1.084	2.13

ΔH , in. H ₂ O	$\frac{\Delta H}{13.6}$	$Y_i = \frac{V_w P_b (t_d + 460)}{V_d (P_b + \frac{\Delta H}{13.6}) (t + 460)}$	$\Delta H \theta_i = \frac{0.0317 \Delta H}{P_b (t_d + 460)} \left[\frac{(t_w + 460) \theta}{V_w} \right]^2$
0.5	0.0368		
1.0	0.0737		
1.5	0.110		
2.0	0.147		
3.0	0.221		
4.0	0.294		

^a If there is only one thermometer on the dry gas meter, record the temperature under t_d .

POSTTEST DRY GAS METER CALIBRATION DATA FORM (English units)

Test number 1 Date 6 Oct 87 Meter box number Autotech Plant Hill AFB
 Barometric pressure, $P_b = 29.379$ in. Hg Dry gas meter number 14931-78005 Pretest $Y = 1.084$

Orifice manometer setting, (ΔH), in. H_2O	Gas volume		Temperature				Y_i	Vacuum setting, in. Hg	Y_i	$\frac{V_w P_b (t_d + 460)}{V_d (P_b + \frac{\Delta H}{13.6})(t_w + 460)}$
	Wet test meter (V_w), ft^3	Dry gas meter (V_d), ft^3	Wet test meter (t_w), $^{\circ}F$	Dry gas meter						
				Inlet (t_{d_i}), $^{\circ}F$	Outlet (t_{d_o}), $^{\circ}F$	Average (t_d), $^{\circ}F$				
1.0	10	90.667	68.2/528.45	73	69	71.25	1.072	13	1.072	
1.0	10	951.277	68.7/528.6	74	72	73.25	1.075	13	1.075	
1.0	10	971.234	68.5/528.7	74	72	73.25	1.077	13	1.077	
										$Y = 1.075$

^a If there is only one thermometer on the dry gas meter, record the temperature under t_d where

V_w = Gas volume passing through the wet test meter, ft^3 .

V_d = Gas volume passing through the dry gas meter, ft^3 .

t_w = Temperature of the gas in the wet test meter, $^{\circ}F$.

t_{d_i} = Temperature of the inlet gas of the dry gas meter, $^{\circ}F$.

t_{d_o} = Temperature of the outlet gas of the dry gas meter, $^{\circ}F$.

t_d = Average temperature of the gas in the dry gas meter, obtained by the average of t_{d_i} and t_{d_o} , $^{\circ}F$.

ΔH = Pressure differential across orifice, in. H_2O .

Y_i = Ratio of accuracy of wet test meter to dry gas meter for each run.

Y = Average ratio of accuracy of wet test meter to dry gas meter for all three runs; tolerance = pretest $Y \pm 0.05Y$.

P_b = Barometric pressure, in. Hg.

θ = Time of calibration run, min.

NOZZLE CALIBRATION DATA FORM

Date 15, 16, 17 July Calibrated by MMO

Nozzle identification number	Nozzle Diameter ^a			ΔD , ^b mm (in.)	D_{avg} ^c
	D_1 , mm (in.)	D_2 , mm (in.)	D_3 , mm (in.)		
0.375 (east)	0.369	0.369	0.368	0.001	0.369
0.500 (west)	0.498	0.497	0.498	0.001	0.498
0.300 (west)	0.299	0.301	0.300	0.002	0.300
0.500 (west)	0.499	0.500	0.500	0.001	0.500

where:

^a $D_{1,2,3}$ = three different nozzles diameters, mm (in.); each diameter must be within (0.025 mm) 0.001 in.

^b ΔD = maximum difference between any two diameters, mm (in.),
 $\Delta D \leq (0.10 \text{ mm}) 0.004 \text{ in.}$

^c D_{avg} = average of D_1 , D_2 , and D_3 .

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Appendix E
CALCULATIONS

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CALCULATIONS

This formula was used to calculate the emission rate, R.

$$R = (K) \frac{W_t V_s A_s (86,400 \times 10^{-6}) P_s}{(V_m \text{ std} + V_w \text{ std}) T_s}$$

- where: W_t = total weight of beryllium collected (micrograms, μg)
- A_s = stack surface area (square feet, ft^2)
- V_s = average stack gas velocity (feet per second, ft/s)
- $V_m \text{ std}$ = dry gas sample volume at standard conditions (29.92 in Hg; 77°F)
- $V_w \text{ std}$ = water vapor volume at standard conditions (cubic feet, ft^3)
- T_s = stack temperature (degrees Rankine, °R)
- P_s = absolute stack gas pressure (inches of mercury, in Hg)
- R = beryllium emission rate (grams per day, g/d)
- K = 17.64 °R/in Hg
- 86,400 = conversion factor (seconds per day)
- 10^{-6} = conversion factor (g/ μg)

OPERATING PARAMETERS

Sample		Wt (μ g)	A _s (ft ²)	V _s (ft/s)	V _m std (m ³)	V _w std (m ³)	T _s (°R)	P _s (in Hg)
East								
Run	1	<1.25	1.35	17.02	73.786	1.11	533.8	24.93
	2	<1.25	1.35	20.97	84.285	0.87	542.3	24.91
	3	<1.25	1.35	30.57	120.846	1.21	547.1	24.88
West								
Run	1	60.86	1.35	11.13	84.879	1.35	537.7	25.18
	2	40.455	1.35	13.03	38.818	1.02	546.2	25.05
	3	246.17	1.35	14.46	100.946	1.31	546.6	25.03

where: Wt = weight

A_s = stack cross-sectional area

V_s = stack velocity

V_m std = meter volume at standard conditions (29.92 in Hg; 77°F)

V_w std = water vapor volume at standard conditions

T_s = stack temperature

P_s = absolute stack gas pressure

EAST STACK CALCULATIONS RUN #1, 2, and 3

XROM METH 5			XROM METH 5			XROM METH 5		
Run Number East 1			Run Number East 2			Run Number East 3		
	Run			Run			Run	
METER BOX Y?			METER BOX Y?			METER BOX Y?		
1.0840	Run		1.0840	Run		1.0840	Run	
DELTA H?			DELTA H?			DELTA H?		
1.7000	Run		2.5500	Run		4.9400	Run	
BAR PRESS ?			BAR PRESS ?			BAR PRESS ?		
24.9200	Run		24.9000	Run		24.8700	Run	
METER VOL ?			METER VOL ?			METER VOL ?		
82.3810	Run		95.8400	Run		139.5490	Run	
MTR TEMP F?			MTR TEMP F?			MTR TEMP F?		
74.9000	Run		85.7000	Run		97.4000	Run	
% OTHER GAS REMOVED BEFORE DRY GAS METER?			% OTHER GAS REMOVED BEFORE DRY GAS METER?			% OTHER GAS REMOVED BEFORE DRY GAS METER?		
0.000	Run		0.000	Run		0.000	Run	
STATIC HOH IN?			STATIC HOH IN?			STATIC HOH IN?		
.0700	Run		.0700	Run		.0700	Run	
STACK TEMP.			STACK TEMP.			STACK TEMP.		
73.8000	Run		82.3000	Run		87.1000	Run	
ML. WATER			ML. WATER			ML. WATER		
23.6200	Run		18.5700	Run		25.7100	Run	
IMP. % HOH = 1.5			IMP. % HOH = 1.0			IMP. % HOH = 1.0		
% HOH = 1.5			% HOH = 1.0			% HOH = 1.0		
% CO ₂			% CO ₂			% CO ₂		
0.0000	Run		0.0000	Run		0.0000	Run	
% OXYGEN			% OXYGEN			% OXYGEN		
21.0000	Run		21.0000	Run		21.0000	Run	
% CO?			% CO?			% CO?		
0.0000	Run		0.0000	Run		0.0000	Run	

XROM METH 5

Run Number
East 1

Run

MOL WT OTHER?
79.0000 Run

Mwd = 28.84
MW WET = 28.68

SQRT PSTS?
6.3359 Run

TIME MIN?
120.0000 Run

NOZZLE DIA?
.3690 Run

STK DIA INCH?
15.7500 Run

* VOL MTR STD = 73.786
STK PRES ABS = 24.93
VOL HOH GAS = 1.11
% MOISTURE = 1.48
MOL DRY GAS = 0.985
% NITROGEN = 79.00
MOL WT DRY = 28.84
MOL WT WET = 28.68
VELOCITY FPS = 17.02
STACK AREA = 1.35
STACK ACFM = 1,381.
* STACK DSCFM = 1,121
% ISOKINETIC = 99.95

XROM METH 5

Run Number
East 2

Run

MOL WT OTHER?
79.0000 Run

Mwd = 28.84
MW WET = 28.73

SQRT PSTS?
7.8096 Run

TIME MIN?
120.0000 Run

NOZZLE DIA?
.3690 Run

STK DIA INCH?
15.7500 Run

* VOL MTR STD = 84.285
STK PRES ABS = 24.91
VOL HOH GAS = 0.87
% MOISTURE = 1.03
MOL DRY GAS = 0.990
% NITROGEN = 79.00
MOL WT DRY = 28.84
MOL WT WET = 28.73
VELOCITY FPS = 20.97
STACK AREA = 1.35
STACK ACFM = 1,702.
* STACK DSCFM = 1,365.
% ISOKINETIC = 93.78

XROM METH 5

Run Number
East 3

Run

MOL WT OTHER?
79.0000 Run

Mwd = 28.84
MW WET = 28.73

SQRT PSTS?
11.3826 Run

TIME MIN?
120.0000 Run

NOZZLE DIA?
.3690 Run

STK DIA INCH?
15.7500 Run

* VOL MTR STD = 120.846
STK PRES ABS = 24.88
VOL HOH GAS = 1.21
% MOISTURE = 0.99
MOL DRY GAS = 0.990
% NITROGEN = 79.00
MOL WT DRY = 28.84
MOL WT WET = 28.73
VELOCITY FPS = 30.57
STACK AREA = 1.35
STACK ACFM = 2,482.
* STACK DSCFM = 1,972
% ISOKINETIC = 93.10

WEST STACK CALCULATIONS RUN #1, 2, 3

XROM METH 5			XROM METH 5			XROM METH 5		
Run Number West 1			Run Number West 2			Run Number West 3		
	Run			Run			Run	
METER BOX Y?			METER BOX Y?			METER BOX Y?		
1.0840	Run		1.0840	Run		1.0840	Run	
DELTA H?			DELTA H?			DELTA H?		
2.4600	Run		.4300	Run		3.9200	Run	
BAR PRESS?			BAR PRESS?			BAR PRESS?		
25.1800	Run		25.0500	Run		25.0300	Run	
METER VOL?			METER VOL?			METER VOL?		
100.8200	Run		44.3410	Run		118.5750	Run	
MTR TEMP F?			MTR TEMP F?			MTR TEMP F?		
116.2500	Run		88.0600	Run		108.9000	Run	
% OTHER GAS REMOVED BEFORE DRY GAS METER?			% OTHER GAS REMOVED BEFORE DRY GAS METER?			% OTHER GAS REMOVED BEFORE DRY GAS METER?		
0.0000	Run		0.0000	Run		0.0000	Run	
STATIC HOH IN?			STATIC HOH IN?			STATIC HOH IN?		
.0400	Run		.0400	Run		.0400	Run	
STACK TEMP.			STACK TEMP.			STACK TEMP.		
77.7000	Run		86.2000	Run		86.6000	Run	
ML. WATER?			ML. WATER?			ML. WATER?		
28.7600	Run		21.6900	Run		27.8300	Run	
IMP. % HOH = 1.6			IMP. % HOH = 2.6			IMP. % HOH = 1.3		
% HOH = 1.6			% HOH = 2.6			% HOH = 1.3		
% CO ₂ ?			% CO ₂ ?			% CO ₂ ?		
0.0000	Run		0.0000	Run		0.0000	Run	
% OXYGEN?			% OXYGEN?			% OXYGEN?		
21.0000	Run		21.0000	Run		21.0000	Run	
% CO?			% CO?			% CO?		
0.0000	Run		0.0000	Run		0.0000	Run	

XROM METH 5

Run Number
West 1

Run

MOL WT OTHER?
79.0000 Run

MWd = 28.84

MW WET = 28.67

SQRT PSTS?
4.1632 Run

TIME MIN?
120.0000 Run

NOZZLE DIA?
.4980 Run

STL DIA INCH?
15.7500 Run

* VOL MTR STD = 84.879
STK PRESABS = 25.18
VOL HOH GAS = 1.35
% MOISTURE = 1.57
MOL DRY GAS = 0.984
% NITROGEN = 79.00
MOL WT DRY = 28.84
MOL WT WET = 28.67
VELOCITY FPS = 11.13
STACK AREA = 1.35
STACK ACFM = 903.
* STACK DSCFM = 735.
% ISOKINETIC = 96.34

XROM METH 5

Run Number
West 2

Run

MOL WT OTHER?
79.0000 Run

MWd = 28.84

MW WET = 28.56

SQRT PSTS?
4.8527 Run

TIME MIN?
120.0000 Run

NOZZLE DIA?
.3000 Run

STK DIA INCH?
15.7500 Run

* VOL MTR STD = 38.818
STK PRES ABS = 25.05
VOL HOH GAS = 1.02
% MOISTURE = 2.56
MOL DRY GAS = 0.974
% NITROGEN = 79.00
MOL WT DRY = 28.84
MOL WT WET = 28.56
VELOCITY FPS = 13.03
STACK AREA = 1.35
STACK ACFM = 1,058.
* STACK DSCFM = 834.
% ISOKINETIC = 106.96

XROM METH 5

Run Number
West 3

Run

MOL WT OTHER?
79.0000 Run

MWd = 28.84

MW WET = 28.70

SQRT PSTS?
5.3965 Run

TIME MIN?
115.00 Run

NOZZLE DIA?
.5000 Run

STK DIA INCH?
15.7500 Run

* VOL MTR STD = 100.946
STK PRES ABS = 25.03
VOL HOH GAS = 1.31
% MOISTURE = 1.28
MOL DRY GAS = 0.987
% NITROGEN = 79.00
MOL WT DRY = 28.84
MOL WT WET = 28.70
VELOCITY FPS = 14.46
STACK AREA = 1.35
STACK ACFM = 1,174.
* STACK DSCFM = 936.
% ISOKINETIC = 93.07

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